Tm-doped fiber laser mode-locked by graphene-polymer composite


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Abstract: We demonstrate mode-locking of a thulium-doped fiber laser operating at 1.94 µm, using a graphene-polymer based saturable absorber. The laser outputs 3.6 ps pulses, with ~0.4 nJ energy and an amplitude fluctuation ~0.5%, at 6.46 MHz. This is a simple, low-cost, stable and convenient laser oscillator for applications where eye-safe and low-photon-energy light sources are required, such as sensing and biomedical diagnostics.

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References and links


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### 1. Introduction

Ultrafast lasers based on thulium (Tm) doped fibers [1–5], operating in the ~2 μm range, are important to address demands for mid-IR sources necessary for a variety of applications, ranging from molecular spectroscopy and biomedical diagnostics, to medicine [6] and remote sensing [7]. The 2 μm region is important because several gas molecules (e.g. CO₂ [8]) have characteristic absorption lines. Since liquid water (main constituent of human tissue) absorbs more strongly at ~2 μm (~100 cm⁻¹) than at ~1.5 μm (~10 cm⁻¹) and ~1 μm (~1 cm⁻¹), ~2 μm laser sources are promising for medical diagnostic and laser surgery [9]. In addition, Light Detection And Ranging (LIDAR) [10] measurements and optical free-space telecommunications [10] can be performed within the 2–2.5 μm atmospheric transparency window [11]. Furthermore, fiber lasers offer advantages compared to solid-state lasers, such as compact geometry, efficient heat dissipation and alignment-free operation [12, 13].

2 μm fiber lasers have been mainly mode-locked using nonlinear polarization evolution.
(NPE) [1] and semiconductor saturable absorber mirrors (SESAMs) [3]. However, these have disadvantages: NPE suffers from bulky construction and environmental sensitivity [1], SESAMs have complex fabrication and packaging and as well as limited bandwidth [14]. Nanotubes and graphene are promising saturable absorbers (SA) due to their favorable properties: ultrafast recovery time [15–17], broadband operation [18, 19], ease of fabrication [18–22] and integration [21, 22] into all-fiber configurations. While, broadband operation can be achieved using a distribution of nanotube diameters [18], this is an intrinsic property of graphene due to the gapless linear dispersion of Dirac electrons [19, 20, 22, 23]. Nanotubes have mode-locked fiber [18, 24–29], waveguide [30, 31], solid-state [32–34] and semiconductor lasers [35], covering from ~0.8 to ~2 µm [21, 22]. Ultrafast pulse generation at 0.8 [36], 1 [37], 1.3 [38] and 1.5 µm [19, 21–23, 39, 40] was demonstrated by exploiting graphene saturable absorbers (GSAs). Refs. [41, 42] reported 2 µm solid-state lasers mode-locked with graphene oxide and chemical vapor deposited (CVD) 1–2 layer graphene. Graphene oxide [43, 44] is fundamentally different from graphene: it is an insulating material with a mixture of sp²/sp³ regions [43, 44], with lots of defects and gap states [44]. Thus, it does not offer in principle the wideband tunability of graphene. CVD graphene, on the other hand, is normally grown at very high temperature on Cu [45] or Ni substrate [46]. Therefore, extra steps are required to transfer graphene to the target substrates for photonic applications. Indeed, graphene can be produced in a variety of ways, ranging from micromechanical cleavage [22], to liquid phase exfoliation (LPE) [47], CVD of hydrocarbons [45, 48], carbon segregation from silicon carbide [49] or metal substrates [50] and chemical synthesis from polyaromatic hydrocarbons [51]. LPE has the advantage of scalability, room temperature processing, and does not require any growth substrate. This produces dispersions that can be easily embedded into polymers to form composites with novel optoelectronic properties to be integrated into various systems [22].

Here, we demonstrate a fiber laser mode-locked using a graphene-polymer composite. It operates at 1.94 µm, with low-noise 3.6 ps pulses. Our results show the potential of GSAs for practical fiber lasers in the mid-IR.

2. Device fabrication and characterization

The graphene-polymer composite is produced as follows: 120 mg of graphite (NGS, Naturgraphit) and 90 mg of sodium deoxycholate (SDC) are sonicated at room temperature. The unexfoliated particles are allowed to settle for 10 minutes, followed by 60 minutes of centrifugation at ~17000 g. The top 70% of the centrifuged dispersion is then used for the composite fabrication. Drops are also placed on Transmission Electron Microscope (TEM) grids for analysis in a high resolution TEM (HRTEM). Combined HRTEM and normal-incidence/tilted angle electron diffraction measurements show that our dispersion has ~66% ≤3-layer flakes (~26% single layer, ~22% bi-layer and ~18% tri-layer). The remainder have less than 10 layers. The dispersion is also drop-cast on Si/SiO₂ for Raman measurements with a Renishaw 1000. 5 ml of dispersion is then mixed with polyvinyl alcohol (PVA) in water (~2 wt%) and centrifuged at ~4000 g. Evaporation at room temperature gives a ~40 µm film; finally, further Raman and absorption measurements are performed.

Figure 1 plots a typical Raman spectrum of a flake deposited on Si/SiO₂. Besides the G and 2D peaks, this has significant D and D’ intensities [52, 53]. We assign the D and D’ peaks to the edges of the submicrometer flakes, rather than a large amount of disorder within the flakes [54]. This is further supported by analyzing the G peak dispersion, Disp(G). In disordered carbons the G peak position, Pos(G), increases with decreasing excitation wavelength, from IR to UV [53]. Thus, Disp(G) = ΔPos(G)/Δλₚ, where λₚ is the laser excitation wavelength, increases with disorder [53, 55]. FWHM(G) always increases with disorder [56]. Hence, combining the intensity ratio of the D and G peaks, I(D)/I(G), with FWHM(G) and Disp(G) al-
allows us to discriminate between edges, and disorder in the bulk of the samples. In the latter case, a higher \( I(D)/I(G) \) would correspond to higher FWHM(G) and Disp(G). By analyzing 30 flakes, we find that the distribution of Disp(G), \( I(D)/I(G) \) and FWHM(G) are not correlated, indicating that the D peak is mostly due to edges. Also, Disp(G) is nearly zero for all samples (compared to \( \geq 0.1 \text{ cm}^{-1} \text{ nm}^{-1} \) expected for disordered carbons [55]). Although 2D is broader than in pristine graphene, it is still a single Lorentzian. This implies that even if the flakes are multilayers, they are electronically decoupled and, to a first approximation, behave as a collection of single layers [57]. Figure 1 compares a typical flake with our graphene-PVA composite and pure PVA. We note that the spectrum of the composite (Fig. 1) is a superposition of that of the flake and PVA. Thus, PVA does not affect the structure of the embedded flakes.

![Raman spectra](image1.png)

**Fig. 1.** Raman spectra of flake on Si/SiO\(_2\), polyvinyl alcohol (PVA), graphene-PVA composite.

![Transmittance graph](image2.png)

**Fig. 2.** Transmittance of PVA and graphene-composite.

Figure 2 plots the transmittance of graphene-PVA compared to pure PVA. The UV peak in graphene-PVA is a signature of the van Hove singularity in the graphene density of states [58]. Strong UV absorption is also observed in pure PVA [59]. By considering the pure PVA absorption, we can estimate that of the graphene component to be \(~50\%\) in the NIR. Given that a monolayer absorbs \(~2.3\%\) [60], we estimate an average \(~21\) layers cross the light path.
The GSA is then prepared by sandwiching 2 mm$^2$ of the composite between two fiber connectors, adhered with index matching gel. The integrated device has $\sim$4 dB ($\sim$60%) total insertion loss.

3. Experimental setup

The laser cavity is schematically shown in Fig. 3. It comprises all-fiber integrated components for an environmentally robust and compact system. A Tm-doped fiber amplifier (TDFA), with integrated optical isolator (ISO), having $\sim$25 dB small signal gain at 1.94 $\mu$m, and a broad gain bandwidth (full width at half maximum, FWHM $\sim$60 nm) is followed by a fiber pigtailed airgap ($\sim$80% insertion loss) used to include a bandpass filter (BPF) for pulse stabilization, with 80% maximum transmission and 11 nm transmission bandwidth, centered $\sim$1.94 $\mu$m. A fused-fiber output coupler (OC) extracts 10% of the light per pass; a polarization controller (PC) allows adjustment of the intra-cavity polarization. We estimate the overall cavity group velocity dispersion to be $-59.7$ ps$^2$ km$^{-1}$, determined from the solitonic spectral sidebands observed when the oscillator was operating without the bandpass filter that was included to stabilize the pulse train.

![Fig. 3. TDFA-Tm-doped fiber amplifier; ISO-isolator; BPF-bandpass filter; OC-output coupler; GSA-graphene-SA; PC-polarization controller](image)

4. Results and discussion

The autocorrelation of the output pulse, and the corresponding optical spectrum are plotted in Fig. 4. Figure 4(a) shows that the pulse temporal profile is well represented by a sech$^2$. The FWHM duration (after deconvolution) is 3.6 ps. The corresponding FWHM spectral width is 2.1 nm, giving a time-bandwidth product $\sim$0.59, indicating low chirp [61]. The output power is $\sim$2 mW. Although the laser operates with negative cavity dispersion, and the pulses are soliton-like, the typical spectral sideband signature of deviation from average soliton operation is not observed, because the soliton length, given by $\zeta_{\text{sol.}} = \frac{\pi}{2} \left| \beta_2 \right|$, is long ($\zeta_{\text{sol.}} \sim$ 300 m) compared to cavity length (31 m $\approx \frac{1}{10} \zeta_{\text{sol.}}$), with $\tau_0$ the pulse duration and $\beta_2$ the group velocity dispersion.

The stability and quality of the generated pulses are evaluated via the radio frequency (RF) spectrum [62]. Figure 5 plots the fundamental and 60th harmonics over long (1 MHz) and short (8 kHz) frequency spans. The long range spectra indicate that the stability is high, with peak to noise-floor ratio limited by our 300 Hz resolution (the noise floor of the analyzer is plotted in red). No sidebands at harmonic cavity frequencies are observed over the 1 MHz span, suggesting good pulse-train stability and no Q-switching instabilities. This is confirmed.
\(\Delta f\) is the resolution bandwidth of the spectrum analyzer. With \(\Delta f\) of the noise band, \(\Delta E\), the energy fluctuations, defined as output pulse energy change divided by average output energy, level pedestal component \(\sim\) cavity frequency (Fig. 6).

The short range spectra (Fig. 5(b,d)), spanning 8 kHz with 30 Hz resolution, reveal a low harmonic on a short range span (8kHz), giving low pulse-to-pulse energy fluctuation \(\Delta E \approx 5 \times 10^{-3}\).

Similarly, when the amplitude noise is low, the timing jitter can be evaluated as [62]:

\[
\frac{\Delta t}{T} = \frac{1}{\pi n} \left[ \frac{\Delta P}{\Delta f_{\text{Res}}} \right]^{1/2},
\]

where \(T\) is the cavity period, \(n\) is the harmonic order. The low-frequency timing jitter (Fig. 5(d)), evaluated at the 60th harmonic with \(\Delta P_{60} = 1.6 \times 10^{-5}\), \(\Delta f = 393\) Hz and \(\Delta f_{\text{Res}} = 30\) Hz, is estimated as \(\Delta t/T = 3.9 \times 10^{-5}\). Given the long cavity period \(T = 155\) ns,
this indicates a low timing jitter $\Delta t \approx 6$ ps.

Our analysis suggests that, despite a very simple cavity consisting of non-polarization maintaining (PM) fiber, the laser emits high-quality pulses with low amplitude fluctuations (0.5%) and relatively low timing jitter $\sim 6$ ps. Although the laser mode-locks without the bandpass filter, the quality of the emitted pulses is compromised, with an increase in the RF noise.

![Fig. 6. (Blue) RF spectrum over 100 MHz, with 3 kHz resolution. (Red) analyzer background.](image)

5. Conclusion

In summary, we reported stable continuous-wave mode-locking of a Tm-doped fiber laser, using a graphene-based saturable absorber. The laser generated 3.6 ps pulses at 6.46 MHz, with $\sim 0.4$ nJ pulse energy, demonstrating the operation of graphene in the mid-IR. This simple all-fiber design supports low noise operation in a small footprint, suitable for packing in a compact single-unit system. In addition, this ultrafast laser could be realized using all-PM fiber components, which should further improve the stability and noise properties [63].

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